



HEAT TRANSFER ANALYSIS BY SIMULATION ON CORRUGATED PLATE HEAT EXCHANGER

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ABSTRACT: The flow field inside the heat exchanger is associated with maximum heat transfer rate with minimum pressure drop. In this investigation, the study is carried out on Corrugated PHE. Plate heat exchanger is a device which is used for many applications such as dairy industries, pharmaceutical industries because of their easy cleaning and maintenance process. During the recent few decades, the use of (PHE) is now spread in to various industries like paper, Dairy industries, Pharmaceutical industries mainly for the process of heating or cooling applications. The reason behind the wide spread of plate heat exchanger in today is because of easy maintenance and cleaning. But it creates high turbulence when compared to the shell and tube heat exchanger. In present studies corrugated plate heat exchanger is considered because of their larger heat transfer surface area and it creates more turbulence when compared to the flat plate heat exchangers.

As the fluid moves through a corrugated Plate heat exchanger, the direction of flow along the length changes continuously, this will show the higher heat transfer coefficient when compared to the flat PHE of similar dimensions. And also the results show that the heat transfer coefficient is higher for a given Reynolds number (55°) corrugation angle when compared to (35°) and (45°) corrugation angles. This is due to the higher turbulence of the fluid generated for the higher corrugation angles. By using computational fluid dynamics the velocity and temperature profiles inside the heat exchanger have been developed using the software. The temperature profiles by simulation and their profiles are presented in the figures.

KEYWORDS: Corrugated Plates, Reynolds Number, Corrugation Angle with ($35^\circ, 45^\circ, 55^\circ$) degrees, Nusselt number, CFD, ANSYS.

1. INTRODUCTION

Recovery of heat from process fluids through heat exchangers is receiving increasing attention by the designers of modern chemical plants. Several types of heat exchangers are now available for wide variety of applications involving high heat transfer performance. Plate Heat Exchangers (PHEs) belong to this category. These are

capable of recovering heat efficiency at low temperature differentials (as low as 1°C) mainly because of high turbulence in such units even at low velocities.

Flat corrugated or embossed standardized plates, arranged to form a package, result in a compact form of a heat exchanger having less weight, requiring less space and providing high heat transfer coefficients. The concept of the

PHE was introduced during the later half of the nineteenth century. Dr. Richard Seligman, founder of APV Group, introduced the first commercially feasible PHE in 1923. The initial designs were similar to plate and frame filter presses and employed cast gunmetal plates. Plates pressed in thin gauge stainless steel were introduced in 1993 primarily for heating applications in dairy, food processing and brewing industries. Due to the ease of cleaning, low liquid holdup and availability to meet the hygienic demand, the PHE has become invaluable in the processing of heat sensitive materials in these industries. The initial designs were limited to operating temperatures up to 100°C and pressure of about 0.3MPa.

2. REVIEW OF LITERATURE

Bassiouny M.K. and Martin H. (1984) made an analytical study to calculate the actual velocity and pressure distribution in both the intake and exhaust conduits of PHE, the flow distribution in the channels between the plates and the total pressure drop. The analysis showed that there is a general characteristic parameter for all the PHEs which determine the flow behavior.

Nishimura Tatsuo et al. (1990) investigated flow patterns and mass transfer characteristics in symmetrical two-dimensional wavy-walled channels at moderate Reynolds number ranging from 20 to 300. They also considered two different wall shapes: sinusoidal wall and arc-shaped wall. Two wall shapes were quite different in the development from laminar to transitional flow. In particular, a new flow structure consisting of a regular three-dimensional flow was observed at a low Reynolds number for the arc-shaped wall. This phenomenon lead to an earlier transition of turbulence as compared with the sinusoidal wall. Mass transfer characteristics of wavy-walled channels differ from those of a straight-walled channel when flow separation occurred. The arc-shaped wall had a larger mass transfer rate than the sinusoidal

wall because of an earlier transition of turbulence.

Roetzel W. et al. (1994) evaluated thermal parameters of plate type heat exchangers using temperature oscillation technique by experimental methods. They presented mathematical model for correcting the thermal penetration effect in plate edgings and thick end plates. Finally, they suggested a series of development to make the method more suitable for plate type heat exchangers.

Blomerius H. and Mitra N.K. (2000) investigated flow field and heat transfer in corrugated ducts from the numerical solutions of the Navier-Stokes equations in the laminar to transitional range of Reynolds numbers (600 - 2000). First, the geometric parameters for the best ratio of heat transfer to pressure drop had been determined for two-dimensional channels. Then for these parameters, flow structure and heat transfer had been investigated for three-dimensional (3-D) channels consisting of corrugated plates. The angles 45 and 90 between the corrugations and the main stream direction were considered. A performance evaluation criterion identifies the 3-D corrugated plate at 45 with the best ratio between heat transfer and pressure drop.

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3. CFD ANALYSIS

3.1 CFD ANALYSIS

CFD is useful for studying fluid flow, heat transfer, chemical reactions etc., by solving mathematical equations. These equations are solved using numerical techniques. It can be effectively used for designing a heat exchanger system from scratch as well as in troubleshooting/optimization. CFD employs a very simple principle of resolving the entire system in small cells or grids and applying governing equations on these discrete elements to find numerical solutions regarding pressure distribution, temperature gradients, flow parameters and the like in a shorter time at a lower cost because of reduced required experimental work.

PARAMETER	DIMENSIONS
Length	40cm
Width	15cm
Test fluid channel spacing	0.5cm
Corrugation angles	35 ⁰ ,45 ⁰ ,55 ⁰

Table 3.1- Dimensions of the PHE

The software package used for the entire numerical analysis is ANSYS CFD Package. The geometry was made using Design modeler tool present in ANSYS Workbench. A minimum value of -15, a maximum value of 15 was provided x axis constraints. Spline tool was used to generate a smooth line through the points associated with the respective angles. Once the line is obtained a 2-dimensional framework is obtained by duplicating the line at the desired intervals. This 2- dimensional framework is converted to a 3- dimensional body with the help of extrude tool. The 3-dimensional geometries created have been shown in the Figs.3.1 to 3.3.

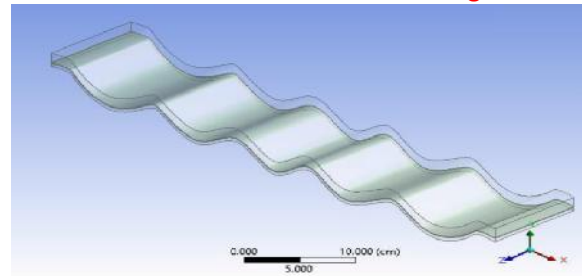


Figure- 3.1 Geometry created for 35⁰ corrugated channel

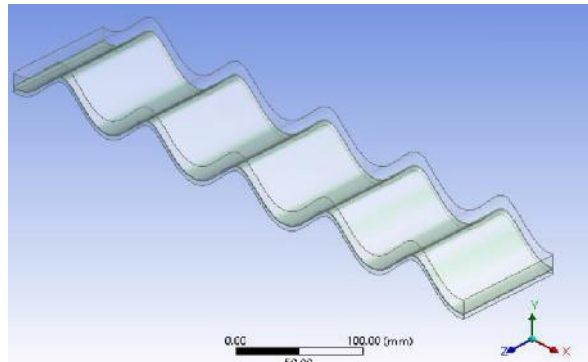


Figure- 3.2 Geometry created for 45⁰ corrugated channel

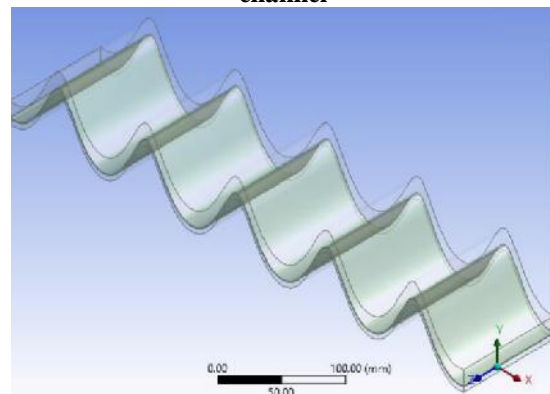


Figure- 3.3 Geometry created for 55⁰ corrugated channel

Parameters	35 ⁰	45 ⁰	55 ⁰
Elements	821762	823718	813720
Orthogonality	0.88	0.81	0.80
Skewness	0.30	0.40	0.52
Mesh mode	CFD	CFD	CFD

Table- 3.2 Mesh Parameters

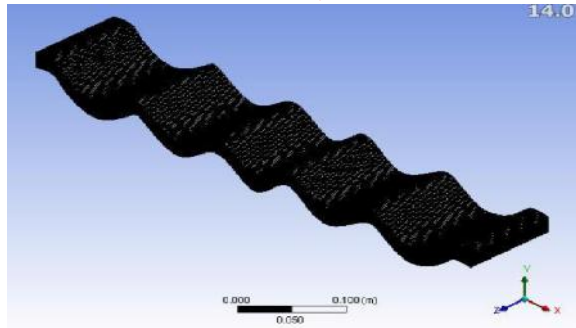


Figure 3.4 Mesh Generated for 35° Corrugated channel

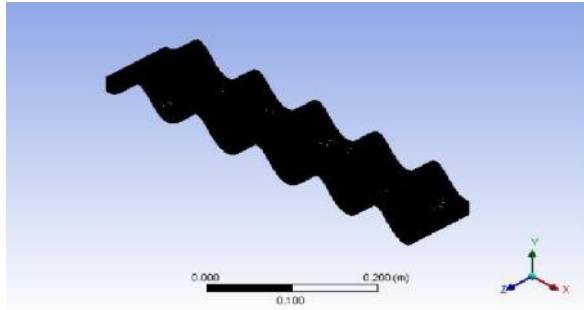


Figure- 3.5 Mesh Generated for 45° Corrugated channel

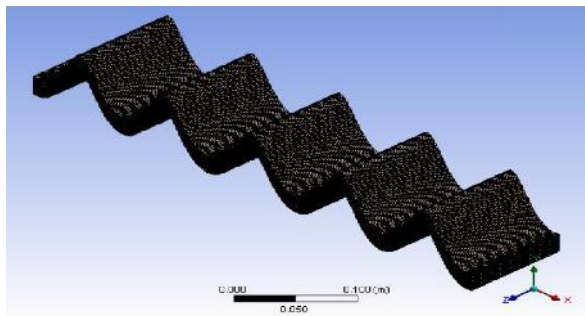


Figure- 3.6 Mesh Generated of 55° Corrugated channel

3.2 Input Conditions to the Model

The governing equations were solved using CFD package FLUENT 14.5 with the following assumptions:

- i. Being a small PHE, there is no mal-distribution of flow.
- ii. Heat transfer surface assumed to be free from fouling. The table 5.3 shows the settings which have been used for model solution in fluent. It is assumed that the flow is uniformly distributed at the entry. Most of the choices are based on previous studies on PHEs.

Function	Specifications
General	Default: Pressure based Steady state.
Viscous	Laminar: Laminar
Material	Fluid : Water- liquid , Solid : Steel from fluent data base.
Cell conditions	Hot fluid : Water. Cold fluid : Water. plate : Stainless Steel.
Boundary conditions	Velocity Magnitude: Hot inlet: 0.0555 m/sec, temperature: 64.6°C (One of the values used) and Other settings are default Cold inlet: Velocity Magnitude: 0.03333m/sec, temperature: 53°C (One of the values used) and Other settings are default
Operating Conditions	Enable gravity option with Y- component value -9.81 m/sec (this settings are made because convection depends on gravity).
Solution Initialization	Hybrid initialization, Initial values: Gauge pressure: 0Pa, X&Y velocity: 0m/sec, Turbulent Kinetic energy: 1m ² /s ² Turbulent dissipation rate: 1 m ² /s. ³

Table- 3.3 Simulation Settings

3.3 Temperature Profiles

The Temperature profiles for Water, 25% Glycerol solution, 35% Glycerol solution and for 35°, 45°, and 55° corrugation angles are shown in Figs. 3.7 to 3.15

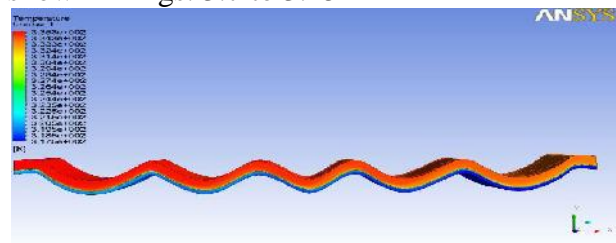


Figure- 3.7 Temperature contours of 35° corrugation angle for Water (3.25lpm)

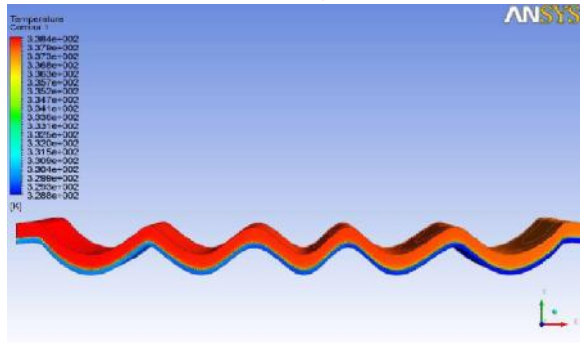


Figure- 3.8 Temperature contours of 35° corrugation angle for 25% Glycerol soln.(3.25lpm)

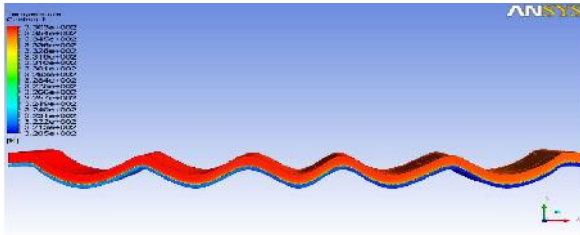


Figure 3.9 Temperature contours of 35° corrugation angle for 35% Glycerol soln.(3.25lpm)

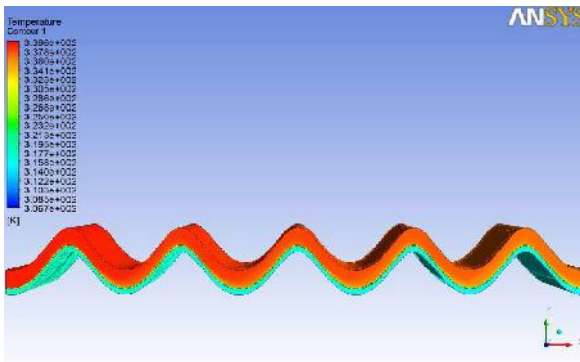


Figure- 3.10 Temperature contours of 45° corrugation angle for (4 lpm)

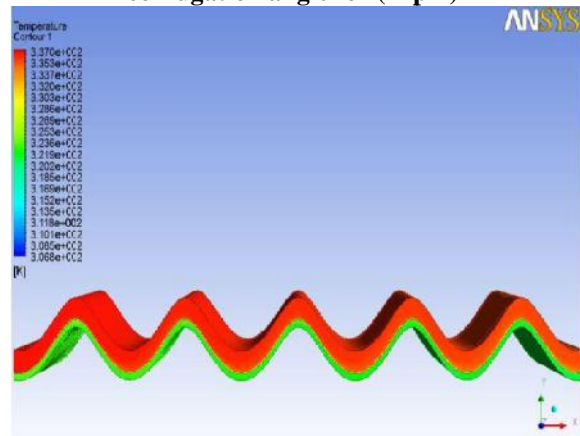


Figure- 3.11 Temperature contours of 45° corrugation angle for 25% Glycerol soln. (4 lpm)

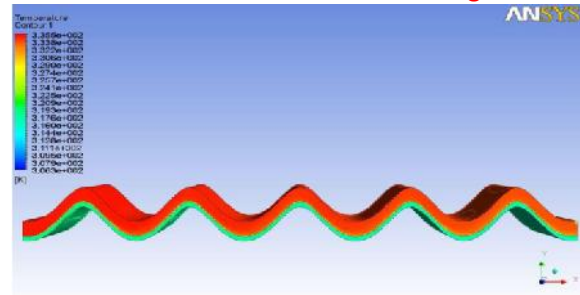


Figure 3.12 Temperature contours of 45° corrugation angle for 35% Glycerol soln. (4lpm)

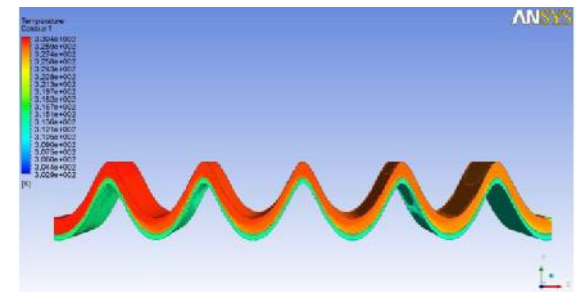


Figure- 3.13 Temperature contours of 55° corrugation angle for Water (4 lpm)

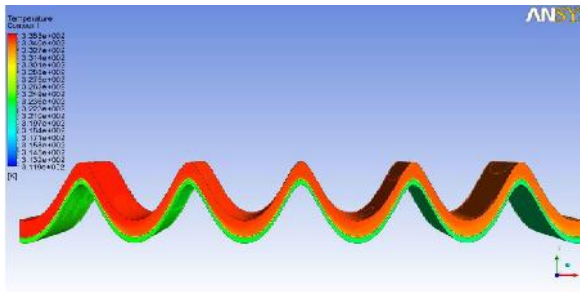


Figure- 3.14 Temperature contours of 55° corrugation angle for 25% Glycerol soln. (4 lpm)

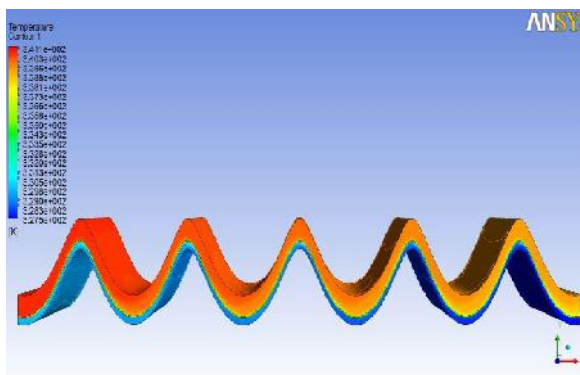


Figure- 3.15 Temperature contours of 55° corrugation angle for 35% Glycerol soln. (4 lpm)

4. RESULTS

Graphs are Drawn for Re and Nu for all the conditions by using the Lab fit software.

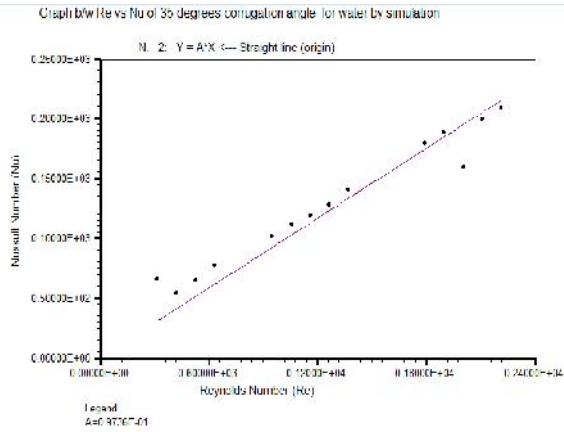


Figure-4.1 Graph b/w Re and Nu for 35 degrees corrugation angle for water

Graph Re vs Nu for 35 degrees corrugation angle for 25% Glycerol by simulation

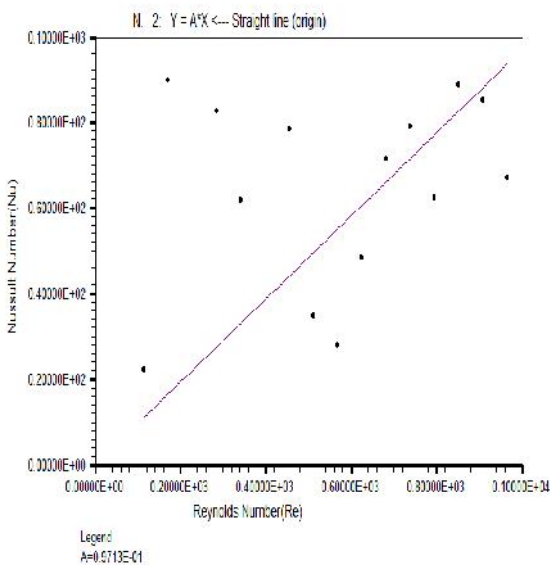


Figure- 4.2 Graph b/w Re and Nu for 35 degrees corrugation angle for 25 % Glycerol by simulation

Graph b/w Re vs Nu of 35 degrees corrugation angle for 35% Glycerol soln by simulation

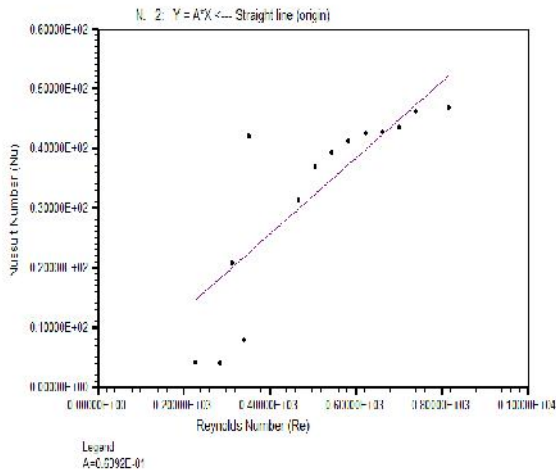


Figure- 4.3 Graph b/w Re and Nu for 35 degrees corrugation angle for 35 % Glycerol by simulation

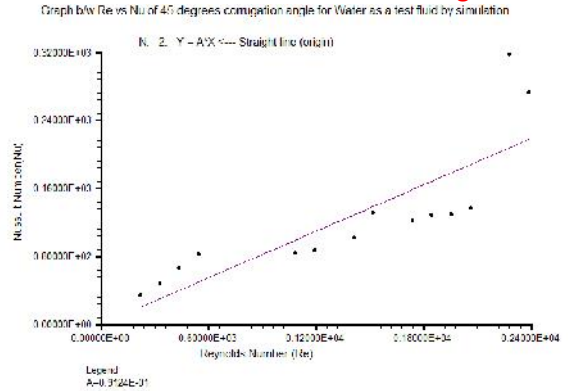


Figure-4.4 Graph b/w Re and Nu for 45 degrees corrugation angle for water

Graph b/w Re vs Nu for 45 degrees corrugation angle for 25% Glycerol soln by simulation

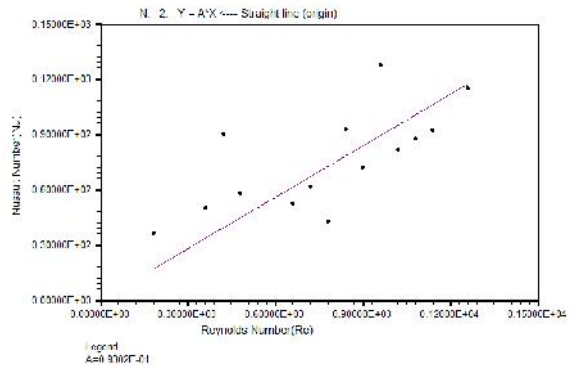


Figure-4.5 Graph b/w Re and Nu for 45 degrees corrugation angle for 25 % Glycerol by simulation

Graph b/w Re vs Nu of 45 degrees corrugation angle for 35% Glycerol soln

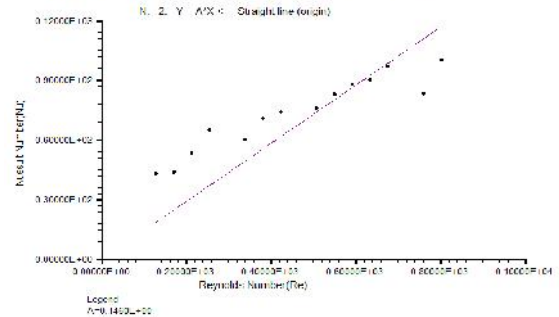


Figure-4.6 Graph b/w Re and Nu for 45 degrees corrugation angle for 35 % Glycerol by simulation

Graph b/w Re vs Nu of 55 degrees corrugation angle for Water by simulation

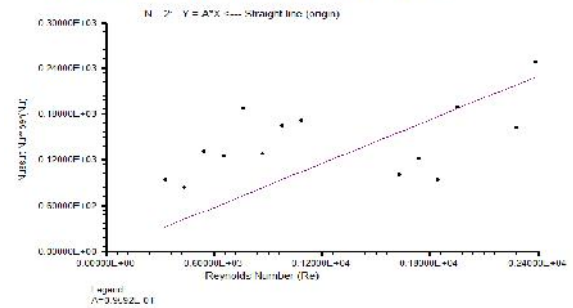


Figure -4.7 Graph b/w Re and Nu for 55 degrees corrugation angle for water

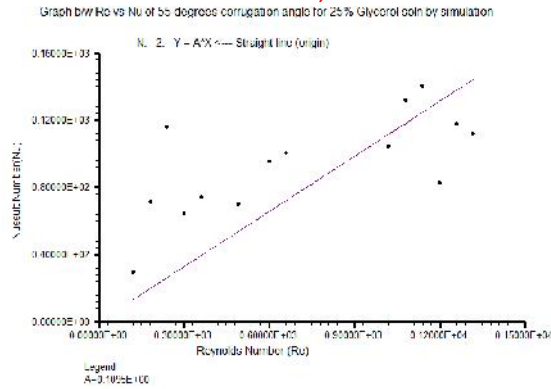


Figure-4.8 Graph b/w Re and Nu for 55 degrees corrugation angle for 25 % Glycerol by simulation

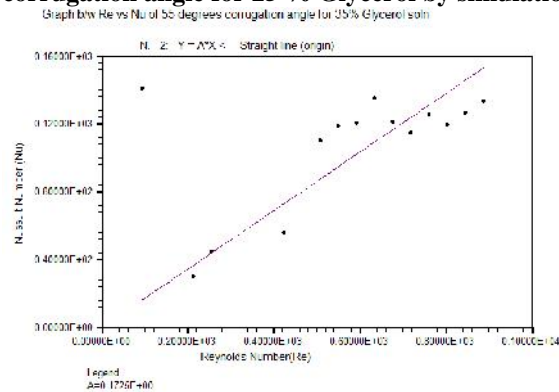


Figure -4.9 Graph b/w Re and Nu for 55 degrees corrugation angle for 35 % Glycerol by simulation

CONCLUSIONS

From the heat transfer studies carried out in the corrugated PHE, the following conclusions are made:

Both heat transfer coefficient and Nusselt number increases with increase in corrugation angle for a particular fluid. It is also inferred from investigation that from 35⁰ to 45⁰ corrugation angle there is an increase in heat transfer rates by 15%, for 45⁰ to 55⁰ corrugation angle there is a 30% increase in heat transfer rates and for 35⁰ to 55⁰ corrugation angle the increase is as high as 50% for all fluids. It can be concluded that with further increase in corrugation angle, the rates of heat transfer that can be achieved will be much higher.

As the corrugation angle increases, there will be significant improvement in the Nusselt number or heat transfer rates for high

viscous fluids compared to low viscous fluids.

Therefore a low viscous fluid at higher corrugation angle will result in same rates of heat transfer compared to high viscous fluids for lower corrugation angles. This aspect can be taken into consideration in choosing the type of corrugated PHE in design.

This is evident from the simulated values good agreement. This model can be used for the simulation of rates of heat transfer for similar type of corrugated PHE by the future investigations.

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